

REMOTE GAZE ESTIMATION USING THE PUPIL CENTER AND CORNEAL REFLECTION

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ABSTRACT

This paper presents the remote estimation of the point-of-gaze (POG) from the coordinates of the centers of the pupil and membrane reflection. Membrane reflection square measure produced by lightweight sources that illuminate the attention and therefore the centers of the pupil and membrane reflection square measure calculable in video pictures from one or a lot of cameras. The covers the total varies of doable system configuration. Exploitation one camera and one lightweight source, the POG may be calculable given that the pinnacle is totally stationary. Exploitation one camera and multiple lightweight sources, the POG can be calculable with free head movements, following the completion of a multiple-point standardization procedure. once multiple cam- eras and multiple lightweight sources square measure used, the POG may be calculable following a straightforward one-point standardization procedure. Experimental and simulation results recommend that the most sources of gaze estimation errors square measure the discrepancy between the form of real corneas and the spherical membrane form assumed within the general theory, and the noise within the estimation of the centers of the pupil and membrane Reflection. An in depth example of a system that uses the final theory to estimate the POG on a monitor is given.

Keywords: Model, Point Of Regard, Pupil Center And Corneal Reflection(S), Remote Gaze Estimation, System Configuration, Video Based Gaze Estimation.

I. INTRODUCTION

The purpose-of-gaze (POG) is that the point in house that's imaged on the middle of the best acuity region of the Retina (fovea) of every eye. Systems that estimate the POG are primarily employed in the analysis of visual scanning patterns and in human-machine interfaces. Since visual scanning patterns closely follow shifts in basic cognitive process focus, they supply insight into human psychological feature processes [1]. As such, analysis of visual scanning patterns is employed within the quantification of mood disorders [2], studies of perception, attention and learning disorders[3], [4], driving analysis and safety [5]–[7], pilot coaching [8], and applied

science [9]. within the space of human-machine interfaces, the POG is used as associate input modality in multimodal human-computer interfaces [10] and helpful devices like gaze-controlled interfaces to permit nonverbal motor-disabled persons to speak and management the atmosphere [11], [12]. There are 2 main categories of gaze estimation systems: head-mounted systems and head-free or remote systems [13]. In head-mounted systems, gaze direction is measured relative to the top. so as to calculate the POG in house, the three-dimensional (3-D) head create (position and orientation) has to be calculable. Numerous kinds of transducers is wont to measure head create, of that the foremost common is that the magnetic position electrical device [14]. Another approach involves the utilization of a head-mounted camera that's wont to record the scene ahead of the topic. Visual cues extracted from pictures obtained by the scene camera are wont to verify the top create relative to the determined scene [15]. Even though head-mounted gaze estimation systems are most popular for applications that need giant and quick head movements, they cannot be employed in applications that need continuous gaze observation over long periods of your time (e.g., aids for motor-disabled persons, observation driver's behavior) or in applications that involve infants. For these applications, remote gaze estimation systems are most popular. Most modern approaches to remote gaze estimation ar primarily based on the analysis of eye options and, sometimes, head options extracted from video pictures.

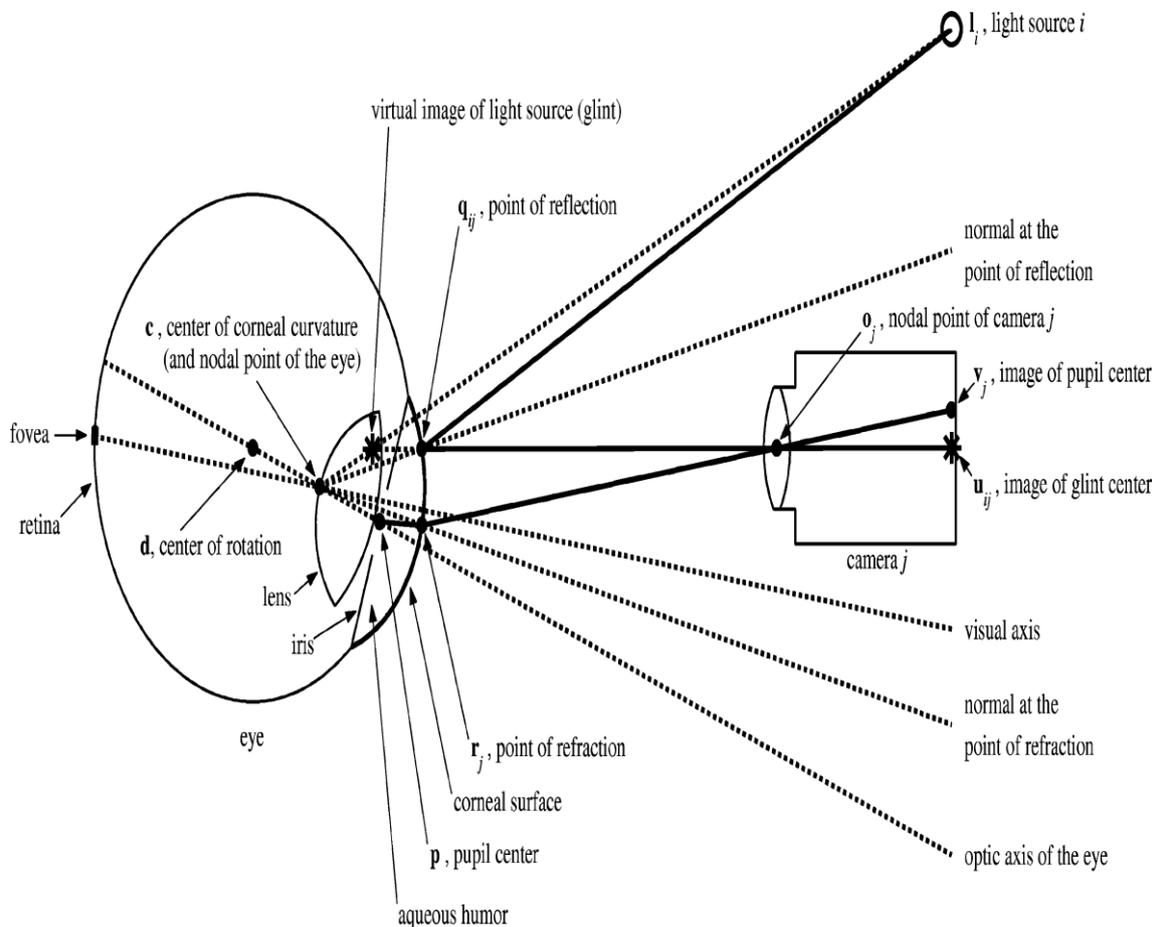


Fig. 1. Ray-tracing diagram (not to scale in order to be able to show all the elements of interest), showing schematic representations of the eye, a camera, and a Light source.

One approach consists of pursuit facial features to estimate the 3D head create and therefore derive the positions of the middle of rotation of the eyes [16], [17]. By combining this info with the calculable positions of the iris or pupil centers, the POG is calculated. Another approach uses the perspective projection of the iris-sclera boundary (limbs) to estimate the position and orientation of the attention in house in order to calculate the POG [18], [19]. the foremost common approach to remote POG estimation uses the estimates of the centers of the pupil and one or additional membrane reflection [7], [11], [13], [20]–[23]. The membrane reflection (first Jan Evangelista Purkinje pictures, glints) are virtual pictures of sunshine sources (usually infrared) that illuminate the attention and are created by the front surface of the cornea that acts as a hogged mirror. The pupil center and corneal reflection(s) are employed in gaze estimation systems for over forty years however a general theory that applies to any or all attainable system configuration and explains the performance, limitations and potential of such systems, isn't offered.

II. MATHEMATICAL MODEL

This section presents a general model for video-based remote POG estimation mistreatment the coordinates of the centers of the pupil and one or additional tissue layer reflection (glints) calculable from pictures captured by one or additional video cameras. The POG is formally defined because the intersection of the visual axes of each eyes with the 3D scene. The visual axis is that the line connecting the center of the region with the nodal purpose of the eye's optics (Fig. 1). Since within the human eye the visual axis deviates from the axis [13], the event that follows is split into two parts. The first half considers the matter of reconstructing the axis of the attention from the centers of pupil and glint(s) in the images of the attention. The second half deals with the reconstruction of the visual axis from the axis, and also the estimation of the POG. 1 Under the assumptions that the sunshine sources are sculptured as point sources and also the video cameras ar sculptured as puncture cameras, Fig. one presents a ray-tracing diagram of the system and the eye, wherever all points are delineated as 3D column vectors (bold font) during a right-handed philosopher world system (WCS). Think about a ray that comes from light

\mathbf{q}_{ij} , and reflects at a degree q_{ij} on the tissue layer surface specified the re- flected ray passes through the nodal purpose of camera \mathbf{q}_{ij} and intersects the camera image plane at a degree j , \mathbf{o}_j . The condition that the ray returning from the purpose of reflection and passing through the nodal purpose of camera intersects the camera image plane at point \mathbf{o}_j , can be expressed in parametric form as

$$\mathbf{q}_{ij} = \mathbf{o}_j + k_{q,ij}(\mathbf{o}_j - \mathbf{u}_{ij}) \text{ for same } k_{q,ij} \quad (1)$$

Whereas, if the corneal surface is modeled as a convex spherical mirror of radius R the condition that \mathbf{q}_{ij} is on the corneal surface can be written as

$$\|\mathbf{q}_{ij} - \mathbf{c}\| = R \quad (2)$$

Where C is the center of corneal curvature.

The law of reflection states two conditions: 1) the incident ray, the reflected ray and the normal at the point of reflection

Are coplanar; 2) the angles of incidence and reflection are equal. Since vector $(q_{ij} - c)$ is normal to the spherical surface at the

point of reflection q_{ij} , condition 1) implies that points $1; q_{ij}, c$ and o_j are coplanar. Noting that three coplanar vectors a_1, a_2 and a_3 satisfy $a_1 \times a_2 \cdot a_3 = 0$, condition 1) can be formalized as

$$(1_j - o_j) \times (q_{ij} - o_j) \cdot (c - o_j) = 0 \quad (3)$$

Since the angle θ between two vectors and can be obtained from $a \cdot b = \|a\| \|b\| \cos \theta$ condition 2) can be expressed as

$$(1_i - q_{ij}) \cdot (q_{ij} - c) \cdot \|o_j - q_{ij}\| = (o_j - q_{ij}) \cdot ((q_{ij} - c)) \|1_i - q_{ij}\| \quad (4)$$

Next, consider a ray that comes from the pupil center P, and refracts at point r_j on the corneal surface such that the refracted ray passes through the nodal point of camera j, o_j and intersects the camera image plane at a point v_j . The condition

That the ray coming from the point of refraction r_j and passing through the nodal point of camera j, o_j intersects the camera

Image plane at point v_j can be expressed in parametric form as

$$x_j = o_j + k_{r,j} (o_j - v_j) \text{ for some } k, j \quad (5)$$

Whereas the condition that x_j is on the corneal surface can be written as

$$\|x_j - c\| = R \quad (6)$$

The law of refraction states two conditions: 1) the incident ray, the refracted ray and the normal at the point of refraction

are coplanar; 2) the angle of incidence θ_1 and the angle of refraction θ_2 satisfy Snell's law (i.e. $n_1 \sin \theta_1 = n_2 \sin \theta_2$ where n_1 and n_2 are the indices of refraction of mediums 1 and 2). Since vector $(x_j - c)$ is normal to the spherical surface at the point of refraction x_j condition 1) implies that points p, r_j, c and o_j are coplanar, which can be formalized as

$$(r_j - o_j) \times (c - o_j) \cdot (p - o_j) = 0 \quad (7)$$

Since the sine of the angle θ between two vectors a and b can be obtained from $\|a \times b\| = \|a\| \|b\| \sin \theta$, condition 2) can be

Expressed as

$$n_1 \cdot \|(r_j - c) \times (p - r_j)\| \cdot \|o_j - r_j\| = n_2 \cdot \|(r_j - c) \times (o_j - r_j)\| \cdot \|p - r_j\| \quad (8)$$

where n_1 is the effective index of refraction of the aqueous humor and cornea combined and n_2 is the index of refraction of air ($\cong 1$).

In this model, the refraction at the aqueous humor cornea interface is neglected since the difference in their indices of refraction is small relative to that of the cornea-air interface. Only the refraction at the cornea-air interface is taken into account and the aqueous humor and cornea are considered as a homogenous medium.

Finally, considering the distance between the pupil center and the center of corneal curvature leads to

$$\|p - c\| = K \quad (9)$$

Since the optic axis of the eye passes through the pupil center (p) and the center of corneal curvature (c), if the above system of equations is solved for c and p, the optic axis of the eye in space can be reconstructed as the line defined by these two points. Notice that in order to solve the above system of equations, the eye parameters R, K and n_1 have to be known. These eye parameters are subject-specific and are not easily measured directly. Therefore, in general, they are obtained through a calibration procedure that is performed for each subject (an example is provided in Section III). The typical values of these eye parameters are given in Appendix A. Since the POG is defined as the intersection of the visual axis rather than the optic axis with the scene, the relation between these two axes has to be modeled. The visual axis is the line

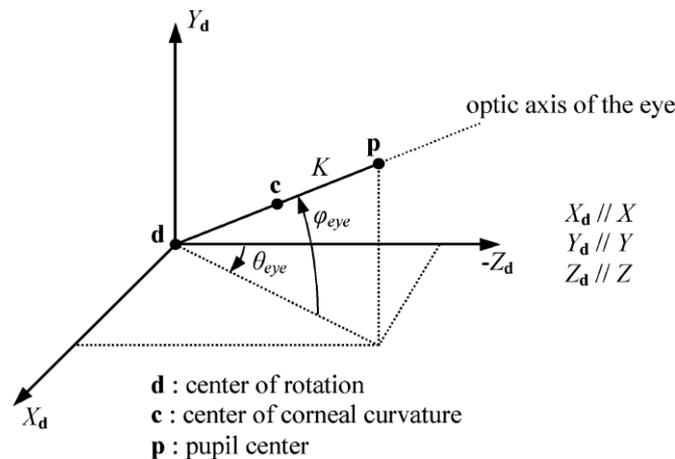


Fig. 2. Orientation of the optic axis of the eye

Defined by the nodal point of the eye and the center of the fovea (i.e., the highest acuity region of the retina corresponding to 0.6 to 1 of visual angle), and deviates from the optic axis [13] (Fig. 1). In a typical adult human eye, the fovea falls about 4–5

Temporally and about 1.5 below the point of intersection of the optic axis and the retina [24].

In order to formalize the relation between the visual and optic axes, suppose that the scene is a vertical plane (e.g., a projection screen or computer monitor) and that the WCS is a right-handed 3-D Cartesian coordinate system whose XY - plane is coincident with the scene plane, with the X-axis horizontal, the Y-axis vertical and the positive Z -axis coming out of the scene plane. Then, the orientation of the optic axis of the eye can be described by the pan (horizontal) angle θ_{eye} and the tilt (vertical) angle ρ_{eye} defined in Fig. 2, where the WCS is translated to the center of rotation of the eye \mathbf{d} . As it can be derived from this figure, the angles θ_{eye} and ρ_{eye} can be obtained from and by solving the following equation:

$$\frac{p-c}{\|p-c\|} = \begin{bmatrix} \cos \rho_{eye} \sin \theta_{eye} \\ \sin \rho_{eye} \\ -\cos \rho_{eye} \cos \theta_{eye} \end{bmatrix} \quad (10)$$

If the horizontal and vertical angles between the visual and optic axes are given by α_{eye} and β_{eye} , respectively, the orientation of the visual axis can be expressed by the pan angle $(\alpha_{eye} + \beta_{eye})$ and the tilt angle ρ_{eye} , where all angles $(\alpha_{eye} + \beta_{eye})$ are signed. In particular, $\alpha_{eye} < 0$ for the right eye while $\alpha_{eye} > 0$ for the left eye, and $\beta_{eye} > 0$. The eye parameters α_{eye} and β_{eye} are subject-specific and are usually estimated through calibration procedure that is performed for each subject. The typical values of these two eye parameters are included in Appendix A.

To completely defined the visual axis in space, in addition to its orientation, a point through which it passes is required. The visual axis and the optic axis intersect at the nodal point of the eye. Since the nodal point remains within 1 mm of the center of corneal curvature for different degrees of eye accommodation [13], for the sake of simplicity, the nodal point is assumed to be coincident with the center of corneal curvature (c). From the above discussion, it follows that the visual axis can be then described in parametric form as

$$c + k_g \begin{bmatrix} \cos(\rho_{eye} + \beta_{eye}) \sin(\theta_{eye} + \alpha_{eye}) \\ \sin(\rho_{eye} + \beta_{eye}) \\ -\cos(\rho_{eye} + \beta_{eye}) \cos(\theta_{eye} + \alpha_{eye}) \end{bmatrix} \quad (11)$$

for all k_g . Since it was assumed that the scene plane $Z = 0$ is at $z = 0$, the POG is given by (11) for a value of k_g . Such that the Z -component of g , equals 0, that is

$$k_g = \frac{c_z}{\cos(\rho_{eye} + \beta_{eye}) \cos(\theta_{eye} + \alpha_{eye})} \quad (12)$$

In the remainder of this Section, it is assumed that the world coordinates of the positions of the light sources ($\mathbf{1}_i$), the nodal point(s) of the camera(s) (\mathbf{o}_j) and the centers of the pupil (\mathbf{v}_j) and glints in the eye images, are known.

Since the centers of the pupil and glints ($u_{i,j}$) that are estimated in each eye image are measured in pixels in an image coordinate system (ICS), they have to be transformed into world coordinates (Appendix B). In order to transform from image coordinates into world coordinates, all camera parameters, including the position of the nodal Point(o_j) must be known. Typically, the camera parameters are estimated through a camera calibration procedure [25], whereas the positions of the light sources are measured directly. In general, the system structure is fixed and, hence, these system parameters are measured/estimated only once during system set up.

The above development shows that 1) the reconstruction of the optic axis of the eye as the line defined by the center of corneal curvature (c) and the pupil center(p) , using (1)–(9), depends on the system configuration (i.e., number of cameras and light sources) and 2) once the optic axis of the eye is obtained, the reconstruction of the visual axis and the estimation of the POG, using (10)–(12), are independent of the system configuration. For this reason, the following subsections concentrate on the reconstruction of the optic axis of the eye for different system configuration, which are presented in order of increasing complexity. The purpose of increasing system complexity is to relax constraints on subject's head movements and simplify the calibration procedure.

2.1 One Camera and One Light Source

The simplest system configuration consists of a single camera and a single light source. In this case, if the eye parameters R, K and are known, the system of equations (1)–(9) with $i=1$ and $j=1$, is equivalent to 13 scalar equations with 14 scalar unknowns. This means that the problem cannot be solved unless another constraint such as

$$\|O_1 - c\| = \text{known} \quad (13)$$

is introduced. This constraint can be satisfied if the head is fixed relative to the system or if the distance between the eye and the camera is estimated somehow (e.g., magnetic head tracker, ultrasonic transducer, auto-focus system, etc.).

In general, gaze estimation systems that use one corneal reflection and one light source do not solve the above system of equations but rather use the vector from the pupil center to the corneal reflection in the eye image to compute the gaze direction relative to the camera axis [13], and either assume that the head movements are negligible or have means to estimate the position of the eye in space (e.g., combination of a moving camera or moving mirrors that track the eye and an auto-focus system or an ultrasonic transducer) [7], [11], [21]–[23]. However, the above system of equations demonstrates the limitations of the single camera-single light source configuration when the head is not completely stationary. The next subsection presents the simplest configuration that allows for the estimation of the POG from the centers of pupil and glints, without any constraints on head movements and without using any additional device to estimate the position of the eye in space.

2.2. One Camera and Multiple Light Sources

The use of multiple light sources allows for the solution of the system of equations (1)–(9) with $i=1, \dots, N-1$ and $j=1$ if the

eye parameters (R, K and n_1) are obtained through a calibration procedure. In this case, it is advantageous to substitute (1) into

(3) to obtain

$$(1_j - o_j) \times (u_{i,j} - o_j) \cdot (c - o_j) = 0. \quad (14)$$

This equation means that the center of corneal curvature c belongs to each plane defined by the nodal point of camera j, o_j light source $i, 1_i$ and its corresponding image point. Moreover, for each camera j all those planes intersect at the line defined by points c and o_j . Since in this case there is only one camera, the subscript that identifies the camera can be dropped for simplicity of notation and, by noting that $a \cdot b = a^T b$, (14), $i=1, \dots, N$ can be written in matrix form as

$$\begin{bmatrix} [(I_1 - o) \times (u_1 - o)]^T \\ \vdots \\ [(I_N - o) \times (u_N - o)]^T \end{bmatrix} (c - o) = 0 \quad (15)$$

From the interpretation of (14) it follows that matrix M has, at most, rank 2. If M has rank 2, the solution to (15) is given by an equation of the form

$$c - o = k_{c,o} b_{norm} \quad (16)$$

Which defined vector $(c-o)$ up to a scale factor. From this reasoning, it follows that (1), (2), (4), $i=1, \dots, N, j=1$ and

(16) are equivalent to $(5N + 3)$ scalar equations with $(4N + 4)$ scalar unknowns. In particular, when $N = 2, b_{norm}$, is a unit

Vector in the direction of the line of intersection of the planes whose normal's are given by $[(I_1 - o) \times (u_1 - o)]$ and $[(I_2 - o) \times (u_2 - o)]$ thus

$$b_{norm} = \frac{b}{\|b\|}$$

$$b = [(I_1 - o) \times (u_1 - o)] \times (I_2 - o) \quad (17)$$

and (1), (2), (4), $i=1,2$ and (16) are equivalent to 13 scalar equations with 12 scalar unknowns.

In the special case that M in (15) has rank 1 [$b=0$ in (17)], which means that all normal's given by $[(I_1 - o) \times (u_1 - o)]$ are Parallel. the effective number of scalar equations decreases to $(5N + 2)$. In the case that $N = 2$, it results in the equivalent to 12 scalar equations with 12 scalar unknowns.

Consequently, if multiple light sources are used, there are enough equations to solve for the center of corneal curvature c . Knowing c , (5) and (6) are used to compute the point of refraction $r = r_1$ (4 scalar unknowns and 4 scalar equations).

Knowing c and r , (7)–(9) are used to compute (3 scalar unknowns and 3 scalar equations). Knowing C and p , the optic axis of the eye can be reconstructed as the line defined by these two points. Notice that the eye parameters R, K and n_1 and must be known in order to reconstruct the optic axis of the eye and thus be able to estimate the POG.

The above discussion shows that one camera and two light sources is the simplest configuration that allows for the reconstruction of the optic axis of the eye from the centers of pupil and glints while allowing for free head movements. The above analysis also shows that knowing c (the center of corneal curvature), the calculation of p (the pupil center) is independent of the number of light sources (7 scalar equations and 7 scalar unknowns regardless of the number of light sources). In the next subsection, system configuration that allow for the reconstruction of the optic axis of the eye without the need for a subject-specific calibration procedure are discussed.

2.3. Multiple Cameras and Multiple Light Sources

When multiple cameras and multiple light sources are used, it is possible to discard all equations that contain the eye parameters R, k and n_1 while still being able to reconstruct the optic axis of the eye by using the remaining equations. In order to keep the notation simple, the discussion that follows is carried out for two cameras, noting that the extension to more cameras is trivial. When two cameras and multiple light sources are used, (14), $i = 1, \dots, N$ and $j = 1, 2$ can be written in matrix form as

$$\begin{bmatrix} [(I_1 - o_1) \times (u_{11} - o_1)]^T \\ [(I_2 - o_2) \times (u_{12} - o_2)]^T \\ \vdots \\ [(I_N - o_1) \times (u_{N1} - o_1)]^T \\ [(I_N - o_2) \times (u_{N2} - o_2)]^T \end{bmatrix} = \begin{bmatrix} (I_1 - o_1) \times (u_{11} - o_1) \cdot o_1 \\ (I_2 - o_2) \times (u_{12} - o_2) \cdot o_2 \\ \vdots \\ (I_N - o_1) \times (u_{N1} - o_1) \cdot o_1 \\ (I_N - o_2) \times (u_{N2} - o_2) \cdot o_2 \end{bmatrix} \quad (18)$$

After applying the distributive property for the dot product, rearranging terms and noting that $a \cdot b = a^T b$. If M_2 has rank 3, c

Can be obtained from (18) by using the left pseudo inverse of M_2 as

$$c = (M_2^T M_2)^{-1} M_2^T h \quad (19)$$

If only 3 linearly independent rows of M_2 and the corresponding rows of h are considered in (18), then (19) reduces to

$$c = M_2^{-1} h.$$

Note that when (5) and (7) are combined, they correspond to the physical condition that for each camera (refer also to Fig. 1),

the pupil center (ρ) the point of refraction r_j , the nodal point of the camera (o_j) the image of the pupil center (v_j), and the Center of corneal curvature (c) are coplanar. For this system configuration with two cameras, it is convenient to represent this

Physical condition as

$$(o_1 - v_1) \times (c - o_1) \cdot (\rho - c) = 0$$

$$(o_2 - v_2) \times (c - o_2) \cdot (\rho - c) = 0 \quad (20)$$

Since the optic axis of the eye is defined by points p and c these equations mean that the optic axis of the eye belongs to the plane defined by points c, o_1 and v_1 (normal given by $[(o_1 - v_1) \times (c - o_1)]$) and to the plane defined by points c, o_2 and v_2 (normal given by $[(o_2 - v_2) \times (c - o_2)]$). Therefore, the optic axis of the eye is the line of the intersection of those two planes and its direction is given by

$$S_{norm} = \frac{s}{\|s\|}$$

$$s = [[(o_1 - v_1) \times (c - o_1)] \times [(o_2 - v_2) \times (c - o_2)]]. \quad (21)$$

If $s \neq 0$ the solution to (20) can be expressed as

$$p - c = k_{pc} S_{norm} \quad (22)$$

which defined vector ($p-c$) up to a scale factor (notice that $|k_{pc}| = K$ the distance between the pupil center and the center of corneal curvature). In this way, knowing c and the direction ($p-c$) of vector s i.e., the direction of vector S , the optic axis of the eye can be reconstructed without actually knowing the eye parameters R, K and n_1 .

III. EXPERIMENT RESULT

This section presents a specific system implementation that is used to estimate the POG on a computer screen. The system utilizes two near-infrared (850 nm) light sources that are symmetrically positioned at the sides of a 19-in computer monitor and a video camera (640× 480 pixels, 1/3-in charge-coupled device with a 35-mm lens) that is centered under the screen. A typical image from the video camera for a subject sitting at a distance of 65 cm from the monitor (typical viewing distance), with his head approximately at the center of the region of allowed head movement, is shown in Fig. 3. This specific system can tolerate only moderate head movements of about ± 3 cm laterally, ± 2 cm vertically, and 4 cm backward/forward, before the eye features are no longer in the field of view of the camera or are out of focus.

To estimate the POG on the screen, a set of system and subject-specific eye parameters has to be measured/estimated. Since the system components are fixed relative to the computer monitor, the system parameters (the position of the two light sources, I_1 and I_2 , and the extrinsic and intrinsic camera parameters, which include the nodal point of the camera, $o = o_1$) are measured/estimated only once during system set up. The

subject-specific eye parameters (R, K, n_1, α_{eye} and β_{eye}) are obtained through a calibration procedure that is performed once for each subject. In the calibration procedure, the subject exits on 9 evenly distributed points that are presented sequentially on the screen. For each fixation point, 100 estimates of the image

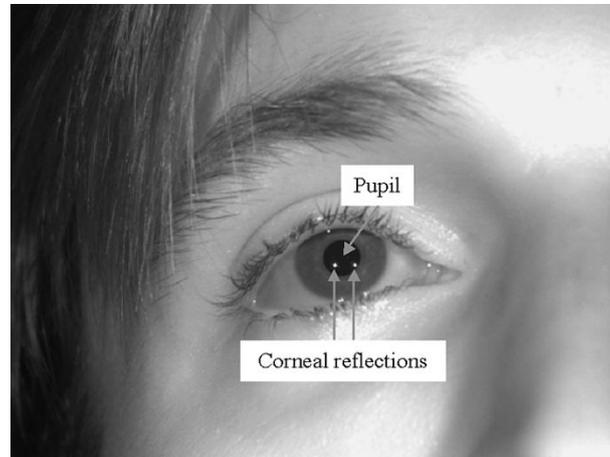


Fig. 3. Sample eye image showing the pupil and the two corneal reflection(glints).

Coordinates of the centers of pupil and glints are obtained and the average coordinates of these features are computed. Using the average coordinates of the centers of pupil and glints, the eye parameters are optimized to minimize the sum of the square errors between the points on the screen and the estimated points-of-gaze [27]. The initial guess for the optimization corresponds to the typical values of the eye parameters given in Appendix A. During the calibration procedure the head is positioned at the center of the region of allowed head movements (central position).

To estimate the POG, the coordinates of the centers of pupil and glints are first estimated in each image captured by the video camera [28]. These image coordinates are then transformed into world coordinates (Appendix B) as $v = v_1$ for the pupil center, and $u_1 = u_{11}$ and $u_2 = u_{21}$ and for the glints. Next, the center of corneal curvature c , is calculated from (1), (2), (4) $i = 1, 2$ and $j = 1$ and (16), (17). Knowing c and r , (5) and (6) are used to compute the point of refraction $r = r_1$. Knowing and , (7)–(9) are used to compute p . Knowing c and p the optic axis of the eye in space is reconstructed as the line defined by these two points. Finally, using (10)–(12), the visual axis of the eye is obtained and the POG on the screen is estimated.

A preliminary evaluation of the performance of this POG estimation system was carried out through experiments with 4 subjects. In these experiments, the head of each subject was placed in the central position and 4 positions at the edges of the region of allowed head movements. The 4 edge positions correspond to lateral and backward/forward head displacements. For each head position, the subject was asked to fixation on 9

points on the computer screen and 100 estimates ($\cong 3.3$ s at 30 estimates/s) of the POG were obtained for each fixation point. The resulting root-mean-square (RMS) errors in the estimation of the POG for the central position and the edge positions are summarized in Table I (RMS error). Table I also shows the RMS errors when the POG was estimated for the average of the coordinates of the centers of pupil and glints (ACPG-RMS error). A typical example of POG estimation errors for the central head position is shown in Fig. 4. The ACPG-RMS errors (Table I) correspond to the deviation of the white crosses from the centers of the dotted circles in Fig. 4 and are the result of bias in the estimation of the POG. The dispersion of the asterisks around the white crosses is caused by noise in the estimates of the image coordinates of the centers of pupil and glints. The RMS errors shown in the last column of Table I correspond to the combined effects of bias and dispersion of the POG estimates. It can be also observed that the RMS errors for the edge head positions are larger than the RMS errors for the central head position.

TABLE I
EXPERIMENTAL RMS POINT-OF-GAZE ESTIMATION ERRORS

Subject	Head position(s)	ACPG-RMS ^a error (mm)	RMS error (mm)
M. E.	Central	2.93	5.15
	Edges	4.25	6.12
J. K.	Central	4.88	6.41
	Edges	5.33	6.73
R. H.	Central	4.93	7.01
	Edges	5.74	7.58
E. G.	Central	4.68	6.25
	Edges	8.12	9.04

^aRMS error when the point-of-gaze was estimated for the average coordinates of the centers of pupil and glints.

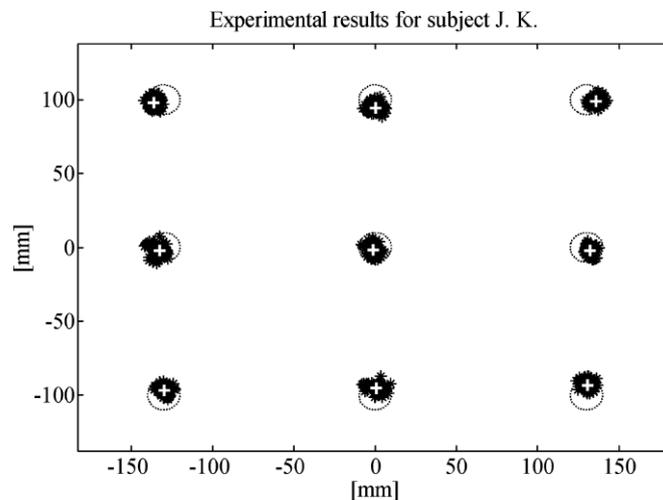


Fig. 4. Experimental POG estimation results for subject J. K. The centers of the dotted circles (10 mm radius) indicate the intended fixation points, the asterisks represent the estimates of the POG, and the

white crosses represent the estimates of the POG for the average coordinates of the centers of pupil and glints.

In order to understand the observed errors, the effects of differences between the shape of real human corneas and the ideal spherical corneal shape assumed in the model of Section II (corneal asphericity), as well as the effects of noise in the estimation of the centers of pupil and glints in the eye images, were studied through numerical simulations. The effects of corneal asphericity were studied using an ellipsoidal corneal model[29]. In this model, the corneal surface is modeled as a section of an ellipsoid that has one of its axes coincident with the optic axis of the eye and whose cross-sections perpendicular to the optic axis are circular. This ellipsoidal corneal model can be completely characterized by the distance between the apex of the cornea and the center of rotation of the eye (13.1 mm—see Appendix A), the radius of curvature at the apex of the cornea (7.8 mm—see Appendix A) and the radius of curvature of the cornea at the boundary with the sclera (at 6 mm from the optic axis, R_6). Using this ellipsoidal corneal model, the image coordinates of the centers of pupil and glints were computed for the same fixation points and the same head positions that

TABLE II
SIMULATION RMS POINT-OF-GAZE ESTIMATION ERRORS

R_6 (mm)	Head position(s)	NFD-RMS ^a error (mm)	RMS error (mm)
7.8 (spherical)	Central	0	3.53
	Edges	0	3.57
8	Central	0.22	3.61
	Edges	0.26	3.68
9	Central	1.27	3.76
	Edges	1.33	3.79
10	Central	2.35	4.14
	Edges	2.45	4.17
11	Central	3.41	4.67
	Edges	3.55	4.87
12	Central	4.46	5.49
	Edges	4.65	5.70
13	Central	5.49	6.37
	Edges	5.74	6.60

^aSimulated noise-free image coordinates of the centers of pupil and glints.

Were used in the experiments. As in the experiments, the central head position was used to calibrate the eye parameters. The Resulting RMS POG estimation errors for different degrees of corneal asphericity (different values of the radius of curvature at the cornea-sclera boundary R_6 ,) are summarized in Table II (NFD-RMS error). These POG estimation errors are only due to the difference between the ellipsoidal corneal model used to calculate the image coordinates of the centers of pupil and glints and the spherical corneal model (Section II) used to estimate the POG. It is clear from Table II that the POG estimation errors increase with the degree of corneal asphericity. In particular, corneal asphericity results in sensitivity to head displacements, making the RMS error for the edge head positions larger than the RMS error for the central head position. Furthermore, the

sensitivity to head displacements also increases with the degree of corneal asphericity. If the cornea were truly spherical, head displacements would have no effect on the POG estimation error.

In order to simulate the effect of noise in the estimates of the centers of pupil and glints in the video images, each coordinate of the centers of pupil and glints obtained with the ellipsoidal corneal model was contaminated with 100 independent realizations of an additive zero-mean Gaussian process with a standard deviation of 0.1 pixel. The properties of the noise were similar to those observed in the system using a stationary artificial eye. As for the noise-free simulations described above, the POG was estimated for the central head position and for the 4 edge head positions. The RM Errors of the POG estimates for different degrees of corneal asphericity are summarized in the last column of Table II (RMS error). Fig. 5 shows simulation results for the central head position and for corneal asphericity R_6 that produces an error pattern that is similar to that of the example in Fig. 4. The bias of the white crosses from the centers of the dotted circles is only due to corneal asphericity. The dispersion of the asterisks around the white crosses is caused by the simulated noise in the estimation of the image coordinates of the centers of pupil and glints. The combined effects of estimation bias and dispersion result in the RMS errors shown in the last column of Table II. It can be observed that the errors obtained through simulations (Fig. 5) are consistent with the experimental errors (Fig. 4). This example clearly demonstrates

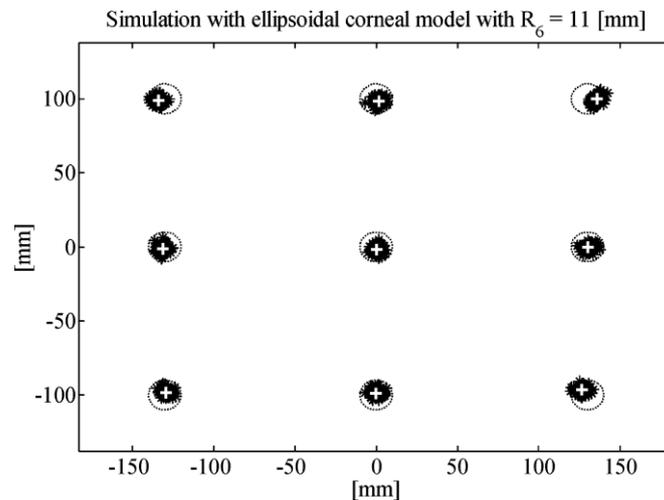


Fig. 5. Simulation results for the ellipsoidal corneal model with $R = 11$ mm The centers of the dotted circles(10 mm radius) indicate the actual fixation points. The white crosses represent the estimates of the POG for the noise-free data. The asterisks represent the estimates of the POG when zero-mean Gaussian noise with a standard deviation of 0.1 pixel was added to the coordinates of the centers of pupil and glints.

IV. CONCLUSION

This paper presented remote POG estimation systems that use the coordinates of the centers of the pupil and corneal reflection (glints) estimated from video images. It was shown that as system complexity (i.e., the number of light sources and the number of cameras) increases, the number of subject-specific parameters that have to be estimated through calibration can be reduced and the constraints on head movements can be relaxed. For a system configuration that consists of one camera and one light source, the POG cannot be determined from the coordinates of the centers of the pupil and the glint, unless the head is stationary or the head position is estimated by some other means.

The simplest configuration that allows for the estimation of the POG, while allowing for free head movements, consists of one camera and two light sources. To estimate the POG with this system configuration, five eye parameters (R, K, n_1, α_{eye} and β_{eye}) have to be estimated through a subject-specific calibration procedure that requires the subject to fixation on multiple points. A specific system implementation that uses one camera and two light sources to estimate the POG on a computer screen was described in detail. It was shown that the main sources of errors in the estimation of the POG are associated with 1) corneal asphericity (deviation of the shape of real corneas from the ideal spherical cornea assumed in the model); and 2) noise in the estimation of the centers of pupil and glints in the eye images. Experimental results obtained with four subjects showed that by Using the general theory, the POG on the computer screen can be estimated with an RMS error of less than 0.9 of visual angle. If at least two cameras and at least two light sources are used, it is possible to reconstruct the optic axis of the eye without a subject-specific calibration procedure (i.e., calibration-free system). In order to reconstruct the visual axis of the eye and thus be able to estimate the POG, the angular deviation between the optic axis and the visual axis (α_{eye} and β_{eye}) still needs to be known. The angular deviation between the optic and visual axes can be estimated through a simple calibration procedure in which the subject is required to fixate on a single point. A single point calibration can be performed even with infants by presenting a flashing object to attract their attention.

A system with two cameras and multiple light sources is under development. Preliminary simulations for a system with two cameras and two light sources (under similar conditions to those described in Section III) yielded RMS POG estimation errors that were less than 7.75 mm (about 0.68 of visual angle). These preliminary results suggest that it is feasible to implement a POG estimation system that requires only a single-point calibration and has an accuracy of 1 of visual angle.

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